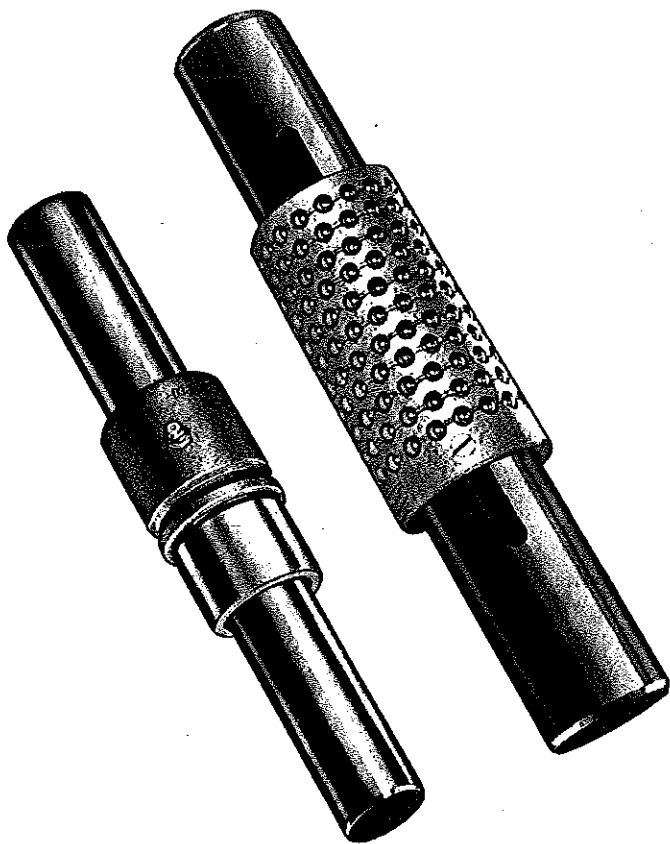




## FACTORS IN DIE SET DESIGN



Today's fierce competition for the diminishing profit return means increasing attention to factors affecting profit and loss. This is true in small and large die shops, in toolrooms, in the stamping industry generally.

Have you reviewed the economic factors in die design and operation recently? And do you know that substantial savings often still can be made on the die designer's bench, in die tryout, in production?

To prove to you how this can be done, we offer information which since it was first published more than ten years ago has accounted for profitable savings to production stampers and die makers alike.

The stamper is interested in uninterrupted high press production. He wants held to a minimum the amount of downtime chargeable to regrinding and die set maintenance and repairs. He also wants scrap held to a minimal level.

Lempico's Ball Bearing Die Sets offer him this opportunity under a general heading of "accuracy". Because a

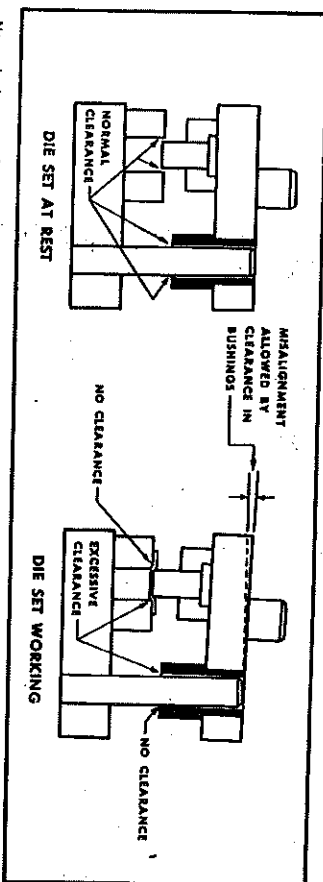
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Lempico Industrial, Inc.

Lempico Ball Bearing Die Set is so accurate there is less die wear, less scrap, less chance of seizure. These are profit factors.

The stamper also should know that less time consumed fitting in the die shop means cost reduction which can result in more favorable pricing. The die maker also should know this because such a saving makes him more competitive. Cost records show that from 30% to 50% of the die maker's time is consumed at the bench—fitting, mounting, aligning. The accuracy of a Lempico Ball Bearing Die Set reduces this time.

Then there's the ease of assembly and disassembly offered by a Lempico Ball Bearing Die Set. How many times are punch holder and die holder assembled, disassembled, reassembled before a new set of dies is ready for trying? Time consumed, times the number of men involved, times the labor cost, can represent important money. If you can reduce this amount substantially, as you can the Lempico ball bearing way, then why not take advantage of your opportunity?

## FACTORS IN DIE SET DESIGN



Normal clearance in a plain bearing die set can allow misalignment, as these sketches show. When working load is applied, normal clearance becomes "redistributed", ranging from zero to an excess. A slight lateral

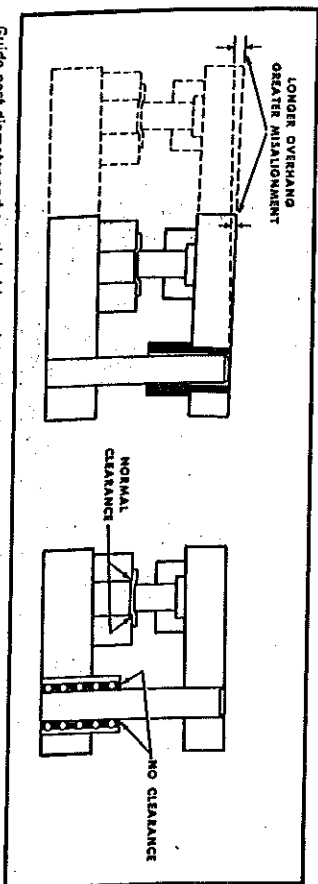
movement results which causes the die to wear faster in one direction. At points of zero clearance there is danger of lubrication breakdown with resulting excessive wear and increasing misalignment.

Alignment of guide posts and bushings, and the clearances provided in fitting them, contribute as much as any other factors to the efficient operation and economic life of a die. The ideal condition would involve a press fit of guide post and bushing (negative clearance), so that the resulting rigidity would assure perfect parallelism between upper and lower die set members under all working stresses.

The pre-loaded ball bearing guide post and bushing offer the accuracy of a press fit and the die set possesses

at the same time an ease of operation which could otherwise be attained only by an impractically large clearance between plain bearing guide post and bushing. Further, the ball bearing assembly presents no lubrication problem such as exists when plain bearing assemblies are fitted with clearances too small for the maintenance of adequate lubrication films. Thus there is less dependence on the press operator for successful die performance since seizure due to inability of lubricant to cover all surfaces is completely eliminated.

(continued next page)



Guide post diameter and punch holder weight determine the overhang that can be tolerated before development of undue binding on plain bearing type posts and bushings. Overhang complicates punch and die alignment. A ball bearing die set maintains perfect closing action

without binding, even under excessive overhang conditions. No misalignment due to clearance or overhang is found in a Lempico Ball Bearing Die Set. A ball bearing set offers free rolling movement vertically, and, therefore, the punch holder can be raised and lowered manually, weight permitting.



# FACTORS IN DIE SET DESIGN

assembly offsets to a marked degree the lack of desirable

When plain bearing assemblies are fitted to closer tolerances, there is an increasing tendency toward binding and galling; this difficulty affects the accuracy with which the punch enters the die. A slight cocking in any direction develops excessive die wear in the direction of displacement. The result is reduced die life overall and more frequent interruptions for regrinding.

Clearance increases with wear in plain bearing assemblies. In a long run involving frequent resharpennings, the total time consumed in resetting becomes a costly non-productive part of the job. A corollary evil stems from the higher rate of rejection due to burrs, mispunches and distortions.

The ball bearing assembly helps solve the problem of alignment which results from situations where large overhangs are required. Under conditions of severe and disproportionate overhang, the "rolling press fit" of the ball bearing assembly enables the upper and lower members of the die set to maintain perfect parallelism at the extremities. In the case of the plain bearing die set, a temporary, although troublesome, solution consists of increasing the diameters of guide posts and bushings. Slowing down the press production rate and exercising greater care to avoid mis-hits also offer additional alleviation of this problem inherent to plain bearing assemblies.

When small shut height reduces the thickness of die shoes, flexing of these members may result with consequent excessive wear on the dies. The ball bearing

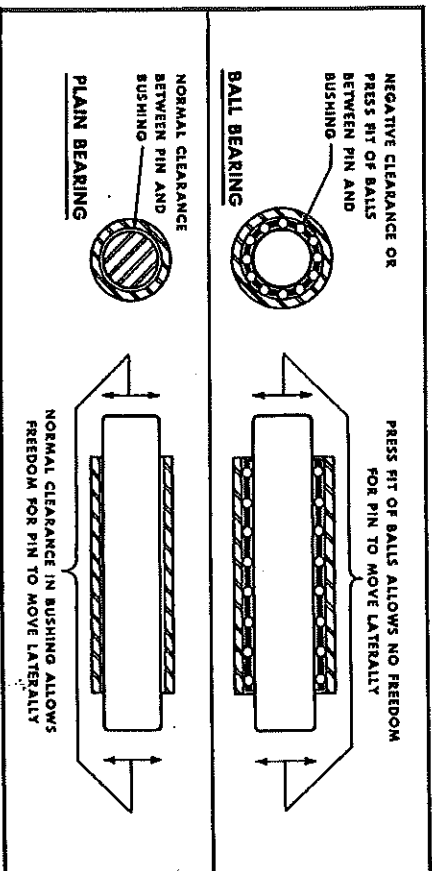
rigidity in die shoes.

Ordinarily a pre-load (negative clearance) would seem conducive to binding, but because of the rolling action of the ball bearings, no such binding exists. The initial pre-load is maintained throughout the longest runs; careful tests have yielded many case histories showing that even after 25 million or more strokes a measurable pre-load still exists.

The success stampers and die makers have had with Lempco's ball bearing assemblies over the course of many years, together with an increasing demand for still greater parts accuracy, have resulted now in introduction of a new and even higher standard of ball bearing die set, Lempco's Precision Grade. The former precision standard now is designated Commercial Grade.

Acceptance of the anti-friction design has established Lempco as a prime source of supply to the stamping industry. In an effort to be of even greater service to the industry, Lempco now makes available a new line of Precision and Commercial Grade Plain Bearing Die Sets. Lempco's Plain Bearing Die Sets are produced with the same quality of manufacture as its Ball Bearing Die Sets. The accuracies of Lempco's new Plain Bearing Die Sets are at least equivalent to those obtained from the best competitive materials available.

Lempco continues to recommend earnestly its Ball Bearing Die Sets for universal application by reason of the economic factors discussed in this article.



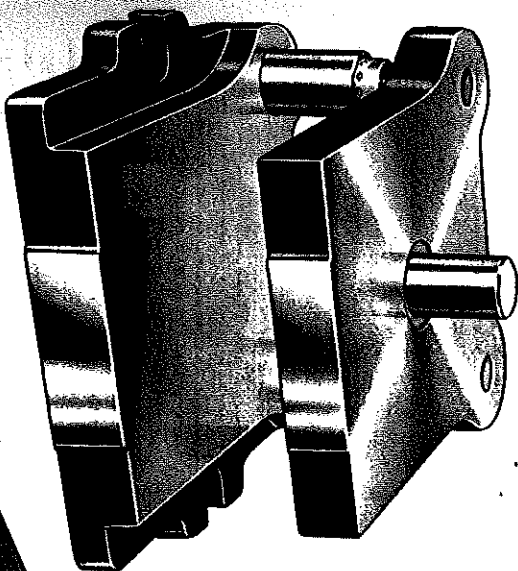
There is no lateral movement in a Lempco Ball Bearing Assembly because of the "rolling press-fit" action. This

is not the case with the plain bearing assembly which requires clearance to function.



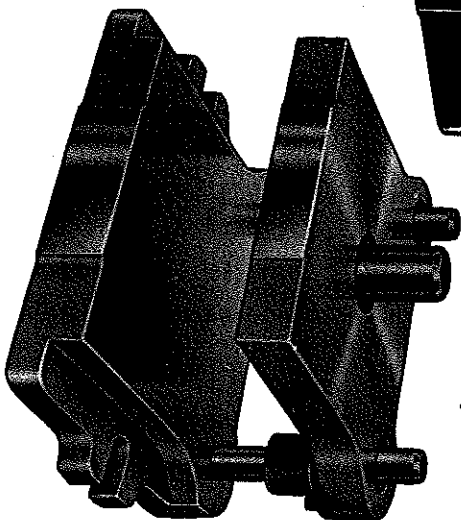
# FLANGED STOCK DIE SETS —Two Post Style

MAY 1, 1967



**BALL BEARING SETS**  
Precision  
Semi-Steel  
Commercial  
Semi-Steel and Steel  
All Steel

**PLAIN BEARING SETS**  
Precision  
Commercial  
Semi-Steel  
All Steel



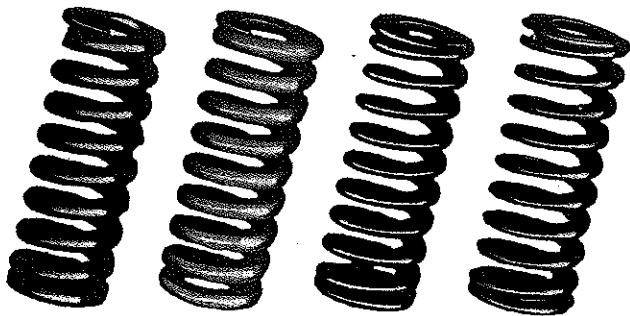
Lempco Ball Bearing and Plain Bearing Two Post Stock Die Sets are offered in both flanged and rectangular designs; the flanged type shown in Catalog Section 1 — Flanged Stock Die Sets—Two Post, and the rectangular in Catalog Section 1A — Rectangular Stock Die Sets—Two Post. Other styles of stock die sets are described in Catalog Section 1B — Rectangular Stock Die Sets—Four Post, Catalog Section 1C — Rectangular Stock Die Sets—Center Post, and Catalog Section 1D — Rectangular Stock Die Sets—Diagonal Post.

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Lempco Industrial, Inc.

Patent Notice—Lempco Ball Bearing Die Sets are manufactured under U. S. Patent No. 2,774,631; Lempco's Die Sets are manufactured under U. S. Patent No. 3,723,941.



**QUALITY DIE SPRINGS**



MEDIUM PRESSURE — BLUE

MEDIUM HEAVY PRESSURE — RED

HEAVY PRESSURE — COPPER

EXTRA HEAVY PRESSURE — GREEN

Lempero's Die Springs represent quality in design, in material, and in manufacturing. Quality controls are strict to assure you of an exceptional Die Spring—unmatched performance.

**CHROME VANADIUM STEEL**

Electric furnace Chrome Vanadium Steel is an extremely tough material. It withstands high stresses, considerable shock, impact loading, and increased deflection. It will operate satisfactorily at higher temperatures than carbon steel.

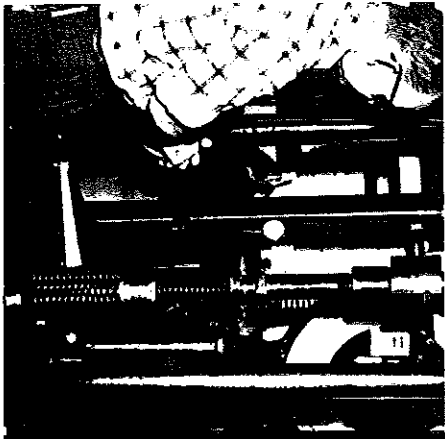
Because of these inherent qualities, Chrome Vanadium Steel is selected as the best material available for Lempero's Die Springs.

**ROUND EDGE WIRE**

Years of research and testing were necessary to achieve an efficient material cross-section and pitch design for Lempero Die Springs. Round edge material was chosen over square edge wire for its increased resistance to fracturing.

**RIGID MATERIAL SPECIFICATIONS**

All material must meet rigid specifications and is labo-



Lempero springs are subjected to many rigorous tests. Here, springs taken from production runs are tested for deflection and for uniformity of tolerances.

**RUGGED DEPENDABLE SERVICE**

factory approved prior to use in production. Any material failing to meet our standard is rejected.

Modern manufacturing facilities assure our customers of uniform springs in size and in deflection tolerances. All Lempero springs are manufactured to the high side of tolerances, to further assure users of proper spring performance.

During manufacture, springs are taken from factory runs and thoroughly tested under working conditions. Springs are subjected to millions of deflection cycles, Rockwell hardness tests, and uniformity tests for all tolerances. Lempero Die Springs are available in four pressure classifications, color-coded for quick visual identification: Blue, Medium Pressure; Red, Medium Heavy Pressure; Copper, Heavy Pressure, and Green, Extra Heavy.

**WIDE SELECTION**

Lempero Die Springs are available in a wide range of sizes, more than 260 in all. Lengths range between 1" and 12", and diameters from 3/8" to 2", one for every common commercial customer requirement. The inherent qualities of Chrome Vanadium Steel combined with the rigid quality controls in design, material,



Springs are tested for millions of deflection cycles under actual working conditions. Tests such as these assure users of long dependable spring operating life.



and production assure you of an exceptional die spring, having high fatigue life, increased deflection, uniform loads and long dependable spring service.

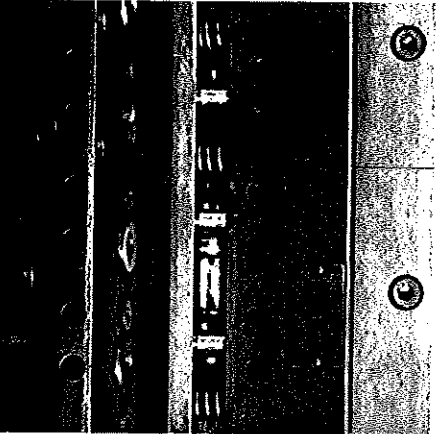
In addition to its Chrome Vanadium line, Lempero also offers for stock delivery a complete assortment of Oil Tempered Machinery Brake and Shear Springs; Carbon Steel Music Wire Die Springs; Carbon Steel Square Wire Die Springs in 12" and 36" lengths, and other compression and extension type springs. Spring Display Panels are available with a wide assortment of springs.

For our customers who require other than catalogued standards, Lempero will supply special compression or extension springs to specifications or print. Special springs are available in an almost infinite variety of design, material, and size combinations.

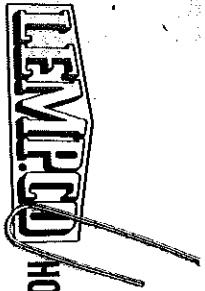
All standard Lempero springs are carried in stock. Strategically located distribution points permit quick shipment. The purpose of this catalog is to assist you in selecting the proper spring from the finest stock available. We are certain that Lempero's standard and special springs will meet all your requirements, and do it with unmatched performance.



Manufacturing processes, such as this coiling operation, produce springs uniform in size and tolerances. Each spring is measured before the succeeding operation, grinding the ends.



A typical die spring application, piercing plate with dies set up in a press brake. Quality springs are a good investment. Their performance is better, insuring against frequent replacement.



## HOW TO SELECT DIE SPRINGS

The following formula will assist you in making the proper spring selection. However, because of variables, some trial-and-error computation may be necessary to select the exact spring best suited for your job.

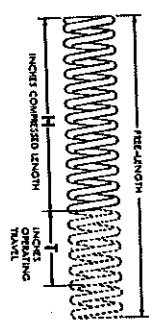
If the spring length and diameter are known, see the tables on Pages 6 to 12 and choose the spring pressure classification and spring with the maximum pressure desired.

Greater delivered spring pressures are realized through the use of longer springs. Longer springs offer more initial loading for "X" travel. Generally, shorter springs develop greater loads at bottom stroke to get even minimum pressures at top stroke, where working spring pressures are actually required.

For maximum spring service, Medium and Medium Heavy Pressure Springs should have a free length equal to five times travel; nine times is desirable for Heavy Pressure. If height limitations necessitate use of shorter springs, the number of springs required will increase accordingly. Rates and total maximum operating deflection can be found on Pages 6 to 12.

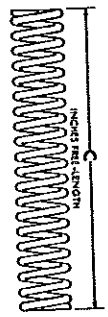
**1**

Determine compressed length of spring "H", and operating travel "T" from your die layout.



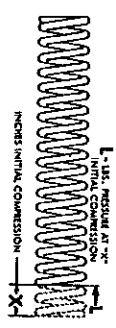
**2**

Determine free length "C" in the following manner: Choose the pressure classification - Medium, Medium Heavy, Heavy, Extra Heavy. Select the desired operating deflection from Long Life, Average Life, or Maximum Deflection (not recommended). Choose the compressed length "H" nearest your die layout requirements. Then read the correlated free length "C" from the tables.



**3**

Calculate total initial spring pressure "L" necessary for all springs when all springs are compressed "X" inches.



**4**

Determine inches of initial compression "X" by using the formula shown below. If "X" is too low, then it is necessary to increase the compressed length "H" in the die.

$$X = C - H - T$$

**5**

Determine rate "R" (total rate for all springs required in pounds per 3/4") by using the formula shown below:

$$R = \frac{L}{8 \times X}$$

**6**

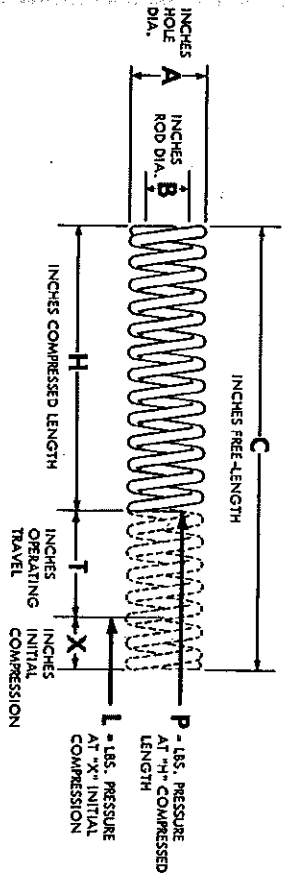
Select springs:  
 A. The free length "C" must agree with the free length determined in Step 2.  
 B. Determine the rate per spring by dividing "R" in Step 5 by the total number of springs to be used, if known.  
 C. Next, see "Loads Required to Deflect 1/4 inch" column in the die spring specifications, Pages 6 to 12, for the catalog number of the spring having the desired rate.  
 To determine the number of springs required (if not known) divide "R" from Step 5 by the rate of the spring you choose.



### TABLE TO CONVERT COMPRESSED LENGTHS TO FREE LENGTHS

C	MEDIUM PRESSURE H COMPRESSED LENGTH			MEDIUM HEAVY PRESSURE H COMPRESSED LENGTH			HEAVY PRESSURE H COMPRESSED LENGTH			EXTRA-HEAVY PRESSURE H COMPRESSED LENGTH		
	Maximum Deflection 30% Comp. (Inches)	Average Life 35% Comp. (Inches)	Long Life 35% Comp. (Inches)	Maximum Deflection 30% Comp. (Inches)	Average Life 35% Comp. (Inches)	Long Life 35% Comp. (Inches)	Maximum Deflection 30% Comp. (Inches)	Average Life 35% Comp. (Inches)	Long Life 35% Comp. (Inches)	Maximum Deflection 30% Comp. (Inches)	Average Life 35% Comp. (Inches)	Long Life 35% Comp. (Inches)
1"	.500	.600	.750	.6300	.7500	.800	.7000	.800	.8500	1.125	1.200	1.275
1 1/4"	.625	.750	.9375	.7875	.9375	1.000	.8750	1.000	1.0540	1.250	1.275	1.300
1 1/2"	.750	.900	1.125	.9450	1.1250	1.200	1.0500	1.200	1.275	1.500	1.600	1.700
2"	1.000	1.200	1.500	1.250	1.500	1.600	1.400	1.600	1.700	1.875	2.000	2.125
2 1/2"	1.250	1.500	1.875	1.575	1.875	2.000	1.750	2.000	2.125	2.125	2.250	2.350
3"	1.500	1.800	2.250	1.890	2.250	2.400	2.100	2.400	2.550	2.550	2.600	2.675
3 1/2"	1.750	2.100	2.625	2.205	2.625	2.800	2.450	2.800	2.975	2.975	3.000	3.075
4"	2.000	2.400	3.000	2.520	3.000	3.200	2.800	3.200	3.400	3.400	3.400	3.425
4 1/2"	2.250	2.700	3.375	2.835	3.375	3.600	3.150	3.600	3.825	3.825	3.800	3.825
5"	2.500	3.000	3.750	3.150	3.750	4.000	3.500	4.000	4.250	4.250	4.200	4.250
5 1/2"	2.750	3.300	4.125	3.465	4.125	4.400	3.850	4.400	4.675	4.675	4.600	4.675
6"	3.000	3.600	4.500	3.780	4.500	4.800	4.200	4.800	5.100	5.100	5.000	5.100
7"	3.500	4.200	5.250	4.410	5.250	5.600	4.900	5.600	5.950	5.950	5.800	5.950
8"	4.000	4.800	6.000	5.040	6.000	6.400	5.600	6.400	6.800	6.800	6.600	6.800
10"	5.000	6.000	7.500	6.300	7.500	8.000	7.000	8.000	8.500	8.500	8.000	8.500
12"	6.000	7.200	9.000	7.560	9.000	9.600	8.400	9.600	10.200	10.200	9.500	10.200

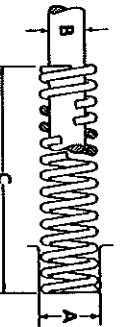
### COMBINED DRAWING FOR STEPS 1-5





MEDIUM PRESSURE DIE SPRINGS

Electric Furnace Chrome Vanadium Steel



All Loads Shown Are Approximate

Table with columns: Hole Diameter (A), Rod Diameter (B), Free Length (C), Catalog Number, Btu Per Hour, Maximum Operating Pressure, Total Deflection, Total Travel. Rows include various spring specifications for 1/2, 3/8, and 1/4 inch diameters.

When ordering please prefix 7001- to catalog number shown.

MEDIUM PRESSURE DIE SPRINGS

Electric Furnace Chrome Vanadium Steel



All Loads Shown Are Approximate

Table with columns: Hole Diameter (A), Rod Diameter (B), Free Length (C), Catalog Number, Btu Per Hour, Maximum Operating Pressure, Total Deflection, Total Travel. Rows include various spring specifications for 1/2, 3/8, and 1/4 inch diameters.

When ordering please prefix 7001- to catalog number shown.

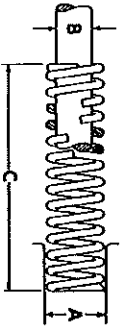






# HEAVY PRESSURE DIE SPRINGS

Electric Furnace Chrome Vanadium Steel



All Loads Shown Are Approximate

Hole Diameter A	Rod Diameter B	Free Length C	Order Number	Rate Per Inch Required to Pull 1/2 Inch	Maximum Operating Deflection		Total Deflection For Service Life		Total Deflection 15% of Length		Total Deflection To Solid	
					Pressure Pounds	Deflection Inches	Pressure Pounds	Deflection Inches	Pressure Pounds	Deflection Inches	Pressure Pounds	Deflection Inches
3/8	3/8	12	9-0804-3	15%	37	.300	25	.200	18.5	.150	44	.334
			9-0606-3	12%	37	.375	24.5	.250	18.5	.1875	45	.463
			9-0508-3	9	43	.450	29	.300	21.5	.225	55	.573
			9-0512-3	5%	45	.750	30	.500	22.5	.375	57	.792
			9-0504-3	1%	43	3.600	29	2.400	22	1.800	70	5.818
1/2	1/2	12	9-0804-3	20%	71	.300	47	.200	35	.150	107	.465
			9-0606-3	23%	70	.375	46.5	.250	35	.1875	109	.587
			9-0508-3	20%	74	.450	49	.300	37	.225	121	.737
			9-0512-3	13%	66	.600	44	.400	33	.300	110	1.000
			9-0504-3	10%	63	.750	42	.500	31.5	.375	106	1.284
5/8	5/8	12	9-0804-3	9%	67	1.050	45	.700	33.5	.525	116	1.810
			9-0606-3	8	58	3.600	38	2.400	29	1.800	100	6.265
			9-0508-3	5%	53	.900	37	.600	31.5	.450	95	1.350
			9-0512-3	26	122	.450	74	.150	55.5	.1875	140	.474
			9-0504-3	13%	94	.600	63	.400	51	.300	165	.696

# HEAVY PRESSURE DIE SPRINGS

Electric Furnace Chrome Vanadium Steel

All Loads Shown Are Approximate



Hole Diameter A	Rod Diameter B	Free Length C	Order Number	Rate Per Inch Required to Pull 1/2 Inch	Maximum Operating Deflection		Total Deflection For Service Life		Total Deflection 15% of Length		Total Deflection To Solid	
					Pressure Pounds	Deflection Inches	Pressure Pounds	Deflection Inches	Pressure Pounds	Deflection Inches	Pressure Pounds	Deflection Inches
2	1	12	9-1604-3	260	624	300	416	200	312	150	614	295
			9-1606-3	148	633	450	335	400	286	225	607	505
			9-1608-3	105	604	600	336	400	282	307	600	774
			9-1610-3	82	510	750	340	500	265	378	629	904
			9-1612-3	59	430	900	326	600	246	400	617	1,134
			9-1614-3	37	479	1,050	319	700	239	525	612	1,343
			9-1616-3	25	480	1,200	320	800	240	600	627	1,553
			9-1618-3	14	475	1,350	317	900	238	675	621	1,763
			9-1620-3	9	468	1,500	312	1,000	234	750	615	1,972
			9-1622-3	5	475	1,650	317	1,100	238	825	628	2,182
			9-1624-3	3	461	1,800	307	1,200	230	900	630	2,392
			9-1626-3	2	470	2,100	314	1,400	230	1,000	650	2,602
1 1/2	1 1/2	12	9-1628-3	24	461	2,400	307	1,600	230	1,200	650	2,811
			9-1632-3	15	438	3,600	288	2,400	216	1,800	589	4,508
			9-2006-3	268	984	450	636	300	477	225	944	490
			9-2008-3	187	898	600	598	400	449	300	933	635
			9-2010-3	147	882	750	588	500	441	375	944	820
			9-2012-3	119	837	900	571	600	428	450	977	1,005
			9-2014-3	94	790	1,050	526	700	395	525	988	1,190
			9-2016-3	83	797	1,200	531	800	396	600	988	1,375
			9-2018-3	73	788	1,350	530	900	394	675	911	1,560
			9-2020-3	62	784	1,500	526	1,000	372	750	866	1,745
			9-2022-3	59	779	1,650	519	1,100	369	825	811	1,930
			9-2024-3	48	763	1,800	509	1,200	362	900	827	2,115
9-2026-3	41	773	2,100	515	1,400	368	1,000	814	2,300			
9-2028-3	38	787	2,400	525	1,600	364	1,100	809	2,485			
9-2030-3	32	768	3,000	512	2,000	354	1,200	820	2,670			
9-2032-3	28	749	3,600	499	2,400	374	1,300	822	4,335			
1 1/4	1 1/4	12	9-2408-3	228	1142	600	782	400	571	300	1346	707
			9-2410-3	166	1116	750	744	500	558	375	1446	892
			9-2412-3	133	1117	900	724	600	551	450	1446	1,179
			9-2414-3	114	1094	1,050	745	700	549	525	1386	1,443
			9-2416-3	88	1094	1,200	720	800	547	600	1386	1,850
			9-2418-3	88	1038	1,350	706	900	529	675	1478	1,850
			9-2420-3	80	1038	1,500	712	1,000	528	750	1510	2,170
			9-2422-3	80	1038	1,650	704	1,100	528	825	1568	2,357
			9-2424-3	72	1031	1,800	701	1,200	526	900	1514	2,592
			9-2426-3	62	1042	2,100	694	1,400	521	1,000	1520	3,064
			9-2428-3	54	1037	2,400	691	1,600	518	1,100	1527	3,535
			9-2430-3	43	1032	3,000	688	2,000	516	1,200	1540	4,477
9-2436-3	36	1037	3,600	691	2,400	518	1,500	1540	5,460			
1 1/2	1 1/2	12	9-3212-3	275	1650	750	1100	400	625	375	1982	901
			9-3214-3	222	1670	900	1104	500	635	450	2129	1,147
			9-3216-3	200	1680	1,050	1220	600	640	525	2227	1,392
			9-3218-3	167	1603	1,200	1060	700	620	600	2168	1,638
			9-3220-3	147	1588	1,350	1046	800	794	675	2216	1,884
			9-3222-3	130	1560	1,500	1030	900	780	750	2214	2,129
			9-3224-3	116	1531	1,650	1021	1,000	786	825	2204	2,375
			9-3226-3	104	1498	1,800	988	1,100	749	900	2187	2,621
			9-3228-3	92	1546	2,100	1030	1,400	773	1,000	2090	3,112
			9-3230-3	80	1536	2,400	1094	1,600	766	1,100	2060	3,605
			9-3236-3	61	1464	3,000	976	2,000	752	1,300	2028	4,589
			9-3248-3	50	1440	3,600	980	2,400	730	1,500	2227	5,588

